



LEE COUNTY BOARD OF ADJUSTMENTS AND APPEALS
Community Development/Public Works Center
1500 Monroe Street, 1st Floor Conference Room 1B

Wednesday, May 18, 2016
10:00 A.M.

AGENDA

CASE TO BE HEARD

Case #ADM2016-00004 (RES2015-00402 & RES2015-00674)

Cowen Residence represented by Tim Krebs, Architect

The applicant is requesting a variance from Section 6-403 LDC and Section R.322.2.1 FBC 5th Edition

1. Call to Order/Review of Affidavit of Publication
2. Roll Call
3. Swearing In of All Testifying
4. Hearing
5. Call the Vote
6. Adjournment

Persons with disabilities who need an accommodation to participate in the Land Development Code Advisory Committee meeting should contact Pam Hendry, 1500 Monroe Street, Fort Myers FL 33901 (239 533-8348 or Phendry@leegov.com). To ensure availability of services, please request accommodation as soon as possible but preferably five or more business days prior to the event. Persons using a TDD may contact Pam Hendry through the Florida Relay Service, 711.

MEMORANDUM
FROM THE
DEPARTMENT OF
COMMUNITY DEVELOPMENT
DEVELOPMENT SERVICES DIVISION

DATE: May 3, 2016

To: BOAA Members

FROM:


Bob Stewart
Building Official

RE: Case #ADM2016-00004 (RES2015-00402 & RES2015-00674) Cowen Residence

This request is for a variance from Section: 6-403 LDC and Section R.322.2.1 FBC 5th Edition requiring lowest floor to meet a base flood elevation of 10.0' NAVD to allow construction of the finished floor at elevation 9.0' NAVD.

This is a non-contributing structure in the Boca Grande Historic District. The project began as an addition and rehabilitation of a 1939 contributing historic structure. During the construction process, the historic part of the existing structure was totally removed. Subsequently, the historic preservation board denied approval of the revisions which replaced the historical cottage with new construction. It was also directed that the historic designation of the building be removed.

At this point the project is approximately two-thirds completed and must be brought into compliance. The completed floor must be elevated to meet the current BFE requirements of 10' NAVD. As constructed, the floor is at 5.0' NVGD.

The applicant has that stated that because of the size of the parcel and the location of the nearly completed structure, it is not possible to meet the required 10' BFE.

Zoning variances have been granted for setbacks from the street which will allow for the building to be elevated to 9' NAVD.

Flood proofing of the residential structure is not allowed and the applicant represents that without the variance, the noncontributing structure would have to be demolished.

In reviewing requests for variances, the Board of Adjustment and Appeals will consider all technical evaluations, all relevant factors, all other applicable provisions of the Florida Building Code, this article, and the following:

- (1) The danger that materials and debris may be swept onto other lands resulting in further injury or damage;
- (2) The danger to life and property due to flooding or erosion damage;
- (3) The susceptibility of the proposed development, including contents, to flood damage and the effect of such damage on current and future owners;

- (4) The importance of the services provided by the proposed development to the community;
- (5) The availability of alternate locations for the proposed development that are subject to lower risk of flooding or erosion;
- (6) The compatibility of the proposed development with existing and anticipated development;
- (7) The relationship of the proposed development to the comprehensive plan and floodplain management program for the area;
- (8) The safety of access to the property in times of flooding for ordinary and emergency vehicles;
- (9) The expected heights, velocity, duration, rate of rise and debris and sediment transport of the floodwaters and the effects of wave action, if applicable, expected at the site; and
- (10) The costs of providing governmental services during and after flood conditions including maintenance and repair of public utilities and facilities such as sewer, gas, electrical and water systems, streets and bridges.

(Ord. No. 15-09, § 1, 5-19-15)

Variances may be issued only upon:

- (1) Submission by the applicant, of a showing of good and sufficient cause that the unique characteristics of the size, configuration, or topography of the site limit compliance with any provision of this article or the required elevation standards;
- (2) Determination by the Board of Adjustment and Appeals that:
 - a. Failure to grant the variance would result in exceptional hardship due to the physical characteristics of the land that render the lot undevelopable; increased costs to satisfy the requirements or inconvenience do not constitute hardship;
 - b. The granting of a variance will not result in increased flood heights, additional threats to public safety, extraordinary public expense, nor create nuisances, cause fraud on or victimization of the public or conflict with existing local laws and articles; and
 - c. The variance is the minimum necessary, considering the flood hazard, to afford relief;
- (3) If the request is for a variance to allow construction of the lowest floor of a new building, or substantial improvement of a building, below the required elevation, a copy in the record of a written notice from the Floodplain Administrator to the applicant for the variance, specifying the difference between the base flood elevation and the proposed elevation of the lowest floor, stating that the cost of federal flood insurance will be commensurate with the increased risk resulting from the reduced floor elevation (up to amounts as high as \$25.00 for \$100.00 of insurance coverage), and stating that construction below the base flood elevation increases risks to life and property.

(Ord. No. 15-09, § 1, 5-19-15)

Staff recommends approval of the variance with the condition that the structure complies with all other elements of the floodplain management regulations.

cc: Terry Lenick, Esquire
Neysa Borkert, Assistant County Attorney

Case #ADM 2016-00004

LEE COUNTY BOARD OF ADJUSTMENTS AND APPEALS APPLICATION

Name: Tim Krebs, Architect

Address: 1460 S. McCall Road, Suite 4A

Phone #: 941-475-7327

Email: tim@takrebs.com

STRAP #: 14432001000600010

Representing: Roy & Holly Cowan RE: 920 Palm Ave, Boca Grande, Florida

IS THIS A ☒ VARIANCE OR ☐ APPEAL? (PLEASE SELECT ONE)

Please provide specific sections of the code or ordinance to which the variance or appeal applies:

BUILDING CODE

COASTAL PLAIN MANAGEMENT

FIRE CODE

FLOOD PLAIN MANAGEMENT X 6-403 LDC + SECTION R.322.2.1 FBC 5TH EDITION

LIFE SAFETY CODE

L.D.C.

MECHANICAL

PLUMBING

If this is an appeal of an administrative decision, please indicate the official who made the decision:

I Request that this matter be scheduled for a hearing before the Lee County Board of Adjustments and Appeals. My reason for this request is as follows: (Provide additional sheets if needed.)

In accordance with 6-81, we seek relief of 1' from the required base flood elevation (required BFE = 10' NAVD, seeking 9') in order to complete the in progress construction at 920 Palm Ave. in accordance with the plans approved by the Boca Grande Historic Preservation Board on April 13, 2016 (See Attached)

I hereby certify that to the best of my knowledge, the information submitted for this hearing is true and correct.

Signature Authorization:  Date: 04-14-16

NOTE: Provide ten (10) copies of all backup information for BOAA members. If there are sealed plans/drawings for the project for which the appeal/variance is requested, the architect/engineer who sealed the plans or drawings **MUST** be present at the hearing.

The applicant's presence is required for a case to be heard by this board.
Hearing dates are usually arranged for Thursday morning at 10:00 a.m.
Applications must be received at least 10 WORKING DAYS before the hearing date.

FEE: \$100.00 - Make check payable to Lee County Board of County Commissioners
This application must be submitted to the Lee County Community Development Permit Center

Revised 12/8/14

s:\committees\boaa\boaa.doc

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COMMUNITY DEVELOPMENT
ADM 2016-00004



East office : 1460 s. McCall rd | ste. 4A | Englewood, Fl 34223
ph: 941 475 7327 | fax : 941 474 0384
West office : 533 N.E. 3rd ave. | ste. 3 | Fort Lauderdale, Fl 33301
ph : 954 999 0488

aa 26002462

www.takrebs.com

April 19, 2016

Variance Request:

Considerations for issuance of Variance:

In reviewing request for variances, the Board of Adjustment and Appeals will consider all technical evaluations, all relevant factors, all other applicable provisions of the Florida Building Code, this article and the following:

(1)The danger that materials and debris may be swept onto other lands resulting in further injury or damage;

The result of a FEMA Hazard Analysis Model program indicates at elevation 9' NAVD no threat exists for the hundred year storm event. The construction includes hydro-static vents for the rise and fall of flood water and includes flood resistant materials below BFE, therefore eliminating the danger of material and debris may be swept onto other lands resulting in further injury or damage.

(2)The danger to life and property due to flooding or erosion damage;

The result of a FEMA Hazard Analysis Model program indicates not threat exists for the hundred year storm event at elevation 9' NAVD. The construction includes hydro-static vents for the rise and fall of flood water and includes flood resistant materials below BFE, therefor eliminating danger to life and property due to flooding or erosion damage.

(3)The susceptibility of the proposed development, including contents, to flood damage and the effect of such damage on current and future owners;

The result of a FEMA Hazard Analysis Model program indicates not threat exists for the hundred year storm event at elevation 9' NAVD. The construction includes hydro-static vents for the rise and fall of flood water and includes flood resistant materials below BFE, therefore eliminating susceptibility of the proposed structure including contents, to flood damage and the effect of such damage on current and future owners.

(4)The importance of the services provided by the proposed development to the community;

The granting of this variance will not impact the services provided to the community.

(5)The availability of alternate locations for the proposed development that are subject to lower risk of flooding or erosion;

This structure is located in accordance with the original 1929 construction and additions thereto. The location as approved by the Boca Grande Preservation Board maintains the Historical Architectural character of the neighborhood.

(6)The compatibility of the proposed development with existing and anticipated development;

The construction maintains the compatibility with the existing Historical neighborhood and development.

(7)The relationship of the proposed development to the comprehensive plan and floodplain management program for the area;

The project is not incompatible with the comprehensive plan or the floodplain management program.

(8)The safety of access to the property in times of flooding for ordinary and emergency vehicles;

The safety and access to the property in times of flooding for ordinary and emergency vehicles will not be impacted by this variance.

(9)The expected heights, velocity, duration, rate of rise and debris and sediment transport of the floodwater and the effects of wave action, if applicable, expected at the site; and

The property is located in an A Zone and as such wave action is not applicable.

(10)The cost of providing governmental services during and after flood conditions including maintenance and repair of public utilities and facilities such as sewer ,gas,electrical and water systems, streets and bridges.

The granting of this variance does not have any impact on any governmental services.

Conditions for issuance of variance:

Variances may be issued only upon:

(1)Submission by the applicant, of a showing of good and sufficient cause that the unique characteristics of the size,configuration, or topography of the site limit compliance with any provision of this article or the required elevation standards;

The requested variance is required to keep the unique historic characteristics of this structure as approved by the Boca Grande Historical Preservation Board.

(2)Determination by the Board of Adjustment and Appeals that:

- (a)Failure to grant the variance would result in exceptional hardship due to the physical characteristics of the land that render the lot underdevelopment;increased cost to satisfy the requirement or inconvenience do not constitute hardship;

Cost or inconvenience is not the basis for granting this variance. The basis is, however the maintenance of the fabric of the Boca Grande Historical district.

- (b)The granting of a variance will not result in increased flood heights, additional threats to public safety, extraordinary public expense, nor create nuisances, cause fraud on or victimization of the public or conflict with existing local law and articles; and

The Building contains hydro-static vents and flood resistant materials below BFE of 9' NAVD as calculated and therefore will not result in increase flood heights, additional threats to public safety, extraordinary public expense, nor create nuisances, cause fraud on or victimization of the public or conflict with existing local laws and articles.

(c)The variance is the minimum necessary, considering the flood hazard, to afford relief;

The variance is the minimum necessary to complete the construction according to the approved plans by the Boca Grande Historical Preservation Board.

(3)If the request is for a variance to allow construction of the lowest floor of a new building, or substantial improvement of a building, below the required elevation, a copy in the record of a written notice from the Floodplain Administrator to the applicant for the variance, specifying the difference between the base flood elevation and the proposed elevation of the lowest floor, stating that the cost of federal flood insurance will be commensurate with the increased risk resulting from the reduced floor elevation (up to amounts as high as \$25.00 for \$100.00 of insurance coverage), and stating that construction below the base flood elevation increases risks to life and property.



Reason for Variance (continue)

The basis for this relief include: the project is surrounded by unique circumstances and without the relief sought the construction will prove contrary to the public interest of preserving the Historic character of the community.

The unique circumstances surrounding this project are as follows:

- #1. The original structure was built in 1930
- #2. The residence received all approvals and permits for rehabilitation and addition and proceeded with construction in March 2015
- #3. The structure has been granted relief of setback requirements preserving it's historic character
- #4. There is virtually no front setback with the front entry wall standing 5.9' from Palm Ave.
- #5. During the course of rehabilitation, it was discovered that all walls, footings and roof required reconstruction for code compliance
- #6. The BGHPB on January 6th 2016 directed staff to begin the process of changing the status of the structure changing from contributing to non-contributing.
- #7. That directive requires the structure to now comply with current flood plain management (BFE 10') and thereby necessitates raising the structure 5' above the original 1930 floor elevation.
- #8. The Owner, Staff, and Architect struggled for a lengthy period seeking a solution which would satisfy the above requirements and the team collectively concluded that 4' was the maximum possible elevation without destroying the historic character of the structure. Furthermore, the Architect has used all techniques to mitigate the additional height approval and creative stair solutions to address the challenges created by the setbacks; He exhausted many options to maintain the historic fabric of the neighborhood and to preserve the character of the community.

To determine whether the granting of this variance would have any adverse effects on the adjacent property owners, the current or future owners or the cost for providing governmental services during or after the 100 year storm event, a FEMA Hazard Analysis Modeling program has been used for this specific site. The results are attached indicates a BFE 9' (as requested). Additionally a storm surge model if applicable indicates 9.6' BFE. In the mapping process FEMA rounds up or down for fractions making this request approximately one tenth of the foot from the storm surge model. Attached are the result of the FHAM.

It is collectively agreed by all parties involved that the variance requested is in the public interest because it protects the historic character of the structure and thus contributes to the fabric of preservation in the Boca Grande Historic district.

Respectively Submitted,

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COMMUNITY DEVELOPMENT

ADM 2016-00004

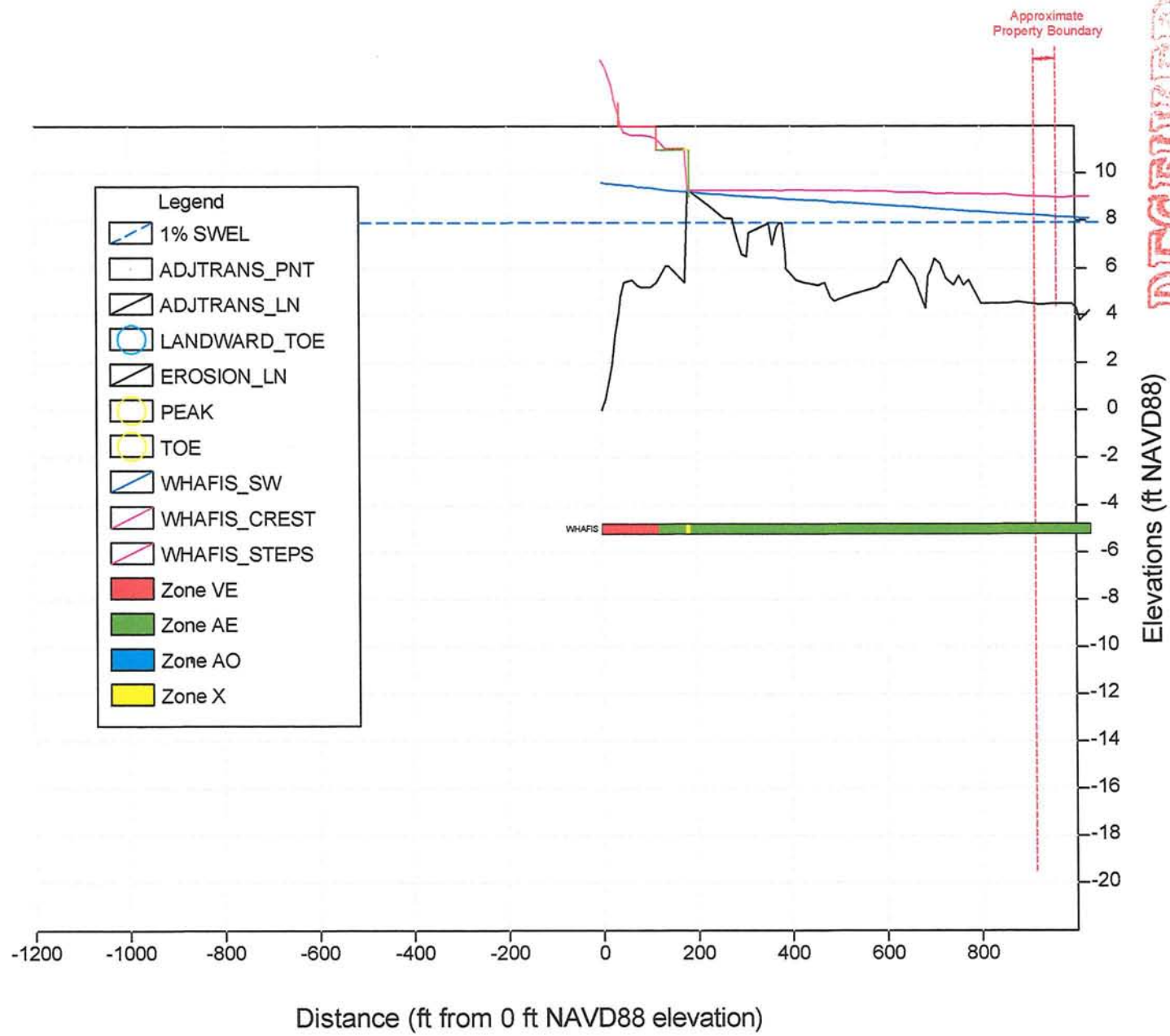


Figure 1 - CHAMP model results - COMPOSITE PROFILE

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COMMUNITY DEVELOPMENT

ADM 2016-00004

- Transect: 1 Date: 3/1/2016
 THIS IS A 100-YEAR CASE

PART1 INPUT

| | | | | | | | | | | |
|----|----------|-------|--------|-------|-------|--------|--------|-------|--------|-------|
| IE | 0.000 | 0.000 | 24.000 | 3.220 | 9.620 | 37.300 | 14.100 | 0.000 | 0.062 | 0.000 |
| IF | 8.000 | 0.500 | 0.000 | 9.602 | 0.000 | 0.000 | 0.000 | 0.000 | 0.090 | 0.000 |
| IF | 21.000 | 1.900 | 0.000 | 9.573 | 0.000 | 0.000 | 0.000 | 0.000 | 0.130 | 0.000 |
| IF | 28.000 | 3.100 | 0.000 | 9.558 | 0.000 | 0.000 | 0.000 | 0.000 | 0.138 | 0.000 |
| IF | 37.000 | 4.100 | 0.000 | 9.538 | 0.000 | 0.000 | 0.000 | 0.000 | 0.142 | 0.000 |
| IF | 40.000 | 4.800 | 0.000 | 9.531 | 0.000 | 0.000 | 0.000 | 0.000 | 0.130 | 0.000 |
| IF | 47.000 | 5.400 | 0.000 | 9.516 | 0.000 | 0.000 | 0.000 | 0.000 | 0.029 | 0.000 |
| IF | 64.000 | 5.500 | 0.000 | 9.478 | 0.000 | 0.000 | 0.000 | 0.000 | -0.004 | 0.000 |
| IF | 75.000 | 5.300 | 0.000 | 9.454 | 0.000 | 0.000 | 0.000 | 0.000 | -0.015 | 0.000 |
| IF | 84.000 | 5.200 | 0.000 | 9.434 | 0.000 | 0.000 | 0.000 | 0.000 | -0.007 | 0.000 |
| IF | 89.000 | 5.200 | 0.000 | 9.423 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| IF | 96.000 | 5.200 | 0.000 | 9.407 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| IF | 103.000 | 5.200 | 0.000 | 9.392 | 0.000 | 0.000 | 0.000 | 0.000 | 0.010 | 0.000 |
| IF | 116.000 | 5.400 | 0.000 | 9.363 | 0.000 | 0.000 | 0.000 | 0.000 | 0.028 | 0.000 |
| IF | 135.000 | 6.100 | 0.000 | 9.321 | 0.000 | 0.000 | 0.000 | 0.000 | 0.027 | 0.000 |
| IF | 142.000 | 6.100 | 0.000 | 9.305 | 0.000 | 0.000 | 0.000 | 0.000 | -0.017 | 0.000 |
| IF | 176.000 | 5.400 | 0.000 | 9.230 | 0.000 | 0.000 | 0.000 | 0.000 | -0.021 | 0.000 |
| AS | 182.000 | 9.300 | 0.000 | 9.230 | 0.000 | 0.000 | 0.000 | 0.000 | -0.021 | 0.000 |
| AS | 185.000 | 9.300 | 0.000 | 9.230 | 0.000 | 0.000 | 0.000 | 0.000 | -0.016 | 0.000 |
| IF | 230.000 | 8.600 | 0.000 | 9.156 | 0.000 | 0.000 | 0.000 | 0.000 | -0.016 | 0.000 |
| IF | 254.000 | 8.200 | 0.000 | 9.116 | 0.000 | 0.000 | 0.000 | 0.000 | -0.016 | 0.000 |
| IF | 261.000 | 8.100 | 0.000 | 9.105 | 0.000 | 0.000 | 0.000 | 0.000 | -0.004 | 0.000 |
| IF | 276.000 | 8.100 | 0.000 | 9.080 | 0.000 | 0.000 | 0.000 | 0.000 | -0.019 | 0.000 |
| IF | 282.000 | 7.700 | 0.000 | 9.073 | 0.000 | 0.000 | 0.000 | 0.000 | -0.075 | 0.000 |
| IF | 288.000 | 7.200 | 0.000 | 9.065 | 0.000 | 0.000 | 0.000 | 0.000 | -0.073 | 0.000 |
| IF | 297.000 | 6.600 | 0.000 | 9.054 | 0.000 | 0.000 | 0.000 | 0.000 | -0.037 | 0.000 |
| IF | 307.000 | 6.500 | 0.000 | 9.042 | 0.000 | 0.000 | 0.000 | 0.000 | 0.060 | 0.000 |
| IF | 312.000 | 7.500 | 0.000 | 9.036 | 0.000 | 0.000 | 0.000 | 0.000 | 0.030 | 0.000 |
| IF | 354.000 | 7.900 | 0.000 | 8.984 | 0.000 | 0.000 | 0.000 | 0.000 | -0.010 | 0.000 |
| IF | 361.000 | 7.000 | 0.000 | 8.976 | 0.000 | 0.000 | 0.000 | 0.000 | -0.070 | 0.000 |
| IF | 364.000 | 7.200 | 0.000 | 8.972 | 0.000 | 0.000 | 0.000 | 0.000 | 0.070 | 0.000 |
| IF | 371.000 | 7.700 | 0.000 | 8.964 | 0.000 | 0.000 | 0.000 | 0.000 | 0.058 | 0.000 |
| IF | 376.000 | 7.900 | 0.000 | 8.958 | 0.000 | 0.000 | 0.000 | 0.000 | 0.018 | 0.000 |
| IF | 382.000 | 7.900 | 0.000 | 8.950 | 0.000 | 0.000 | 0.000 | 0.000 | -0.092 | 0.000 |
| IF | 389.000 | 6.700 | 0.000 | 8.942 | 0.000 | 0.000 | 0.000 | 0.000 | -0.211 | 0.000 |
| IF | 391.000 | 6.000 | 0.000 | 8.939 | 0.000 | 0.000 | 0.000 | 0.000 | -0.054 | 0.000 |
| IF | 411.000 | 5.500 | 0.000 | 8.915 | 0.000 | 0.000 | 0.000 | 0.000 | -0.016 | 0.000 |
| IF | 428.000 | 5.400 | 0.000 | 8.894 | 0.000 | 0.000 | 0.000 | 0.000 | -0.004 | 0.000 |
| IF | 458.000 | 5.300 | 0.000 | 8.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| IF | 472.000 | 5.400 | 0.000 | 8.840 | 0.000 | 0.000 | 0.000 | 0.000 | -0.019 | 0.000 |
| IF | 484.000 | 4.800 | 0.000 | 8.823 | 0.000 | 0.000 | 0.000 | 0.000 | -0.038 | 0.000 |
| IF | 493.000 | 4.600 | 0.000 | 8.811 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 |
| IF | 531.000 | 4.900 | 0.000 | 8.759 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 | 0.000 |
| IF | 583.000 | 5.200 | 0.000 | 8.687 | 0.000 | 0.000 | 0.000 | 0.000 | 0.008 | 0.000 |
| IF | 596.000 | 5.400 | 0.000 | 8.669 | 0.000 | 0.000 | 0.000 | 0.000 | 0.009 | 0.000 |
| IF | 605.000 | 5.400 | 0.000 | 8.657 | 0.000 | 0.000 | 0.000 | 0.000 | 0.021 | 0.000 |
| IF | 615.000 | 5.800 | 0.000 | 8.643 | 0.000 | 0.000 | 0.000 | 0.000 | 0.043 | 0.000 |
| IF | 626.000 | 6.300 | 0.000 | 8.628 | 0.000 | 0.000 | 0.000 | 0.000 | 0.032 | 0.000 |
| IF | 634.000 | 6.400 | 0.000 | 8.617 | 0.000 | 0.000 | 0.000 | 0.000 | -0.007 | 0.000 |
| IF | 640.000 | 6.200 | 0.000 | 8.609 | 0.000 | 0.000 | 0.000 | 0.000 | -0.027 | 0.000 |
| IF | 645.000 | 6.100 | 0.000 | 8.602 | 0.000 | 0.000 | 0.000 | 0.000 | -0.030 | 0.000 |
| IF | 650.000 | 5.900 | 0.000 | 8.595 | 0.000 | 0.000 | 0.000 | 0.000 | -0.029 | 0.000 |
| IF | 662.000 | 5.600 | 0.000 | 8.578 | 0.000 | 0.000 | 0.000 | 0.000 | -0.046 | 0.000 |
| IF | 685.000 | 4.300 | 0.000 | 8.547 | 0.000 | 0.000 | 0.000 | 0.000 | -0.023 | 0.000 |
| IF | 688.000 | 5.000 | 0.000 | 8.543 | 0.000 | 0.000 | 0.000 | 0.000 | 0.233 | 0.000 |
| IF | 691.000 | 5.700 | 0.000 | 8.538 | 0.000 | 0.000 | 0.000 | 0.000 | 0.112 | 0.000 |
| IF | 696.000 | 5.900 | 0.000 | 8.532 | 0.000 | 0.000 | 0.000 | 0.000 | 0.050 | 0.000 |
| IF | 705.000 | 6.400 | 0.000 | 8.519 | 0.000 | 0.000 | 0.000 | 0.000 | 0.014 | 0.000 |
| IF | 717.000 | 6.200 | 0.000 | 8.503 | 0.000 | 0.000 | 0.000 | 0.000 | -0.035 | 0.000 |
| IF | 728.000 | 5.600 | 0.000 | 8.487 | 0.000 | 0.000 | 0.000 | 0.000 | -0.033 | 0.000 |
| IF | 744.000 | 5.300 | 0.000 | 8.465 | 0.000 | 0.000 | 0.000 | 0.000 | 0.004 | 0.000 |
| IF | 756.000 | 5.700 | 0.000 | 8.449 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| IF | 766.000 | 5.300 | 0.000 | 8.435 | 0.000 | 0.000 | 0.000 | 0.000 | -0.009 | 0.000 |
| IF | 777.000 | 5.500 | 0.000 | 8.420 | 0.000 | 0.000 | 0.000 | 0.000 | -0.022 | 0.000 |
| IF | 802.000 | 4.500 | 0.000 | 8.389 | 0.000 | 0.000 | 0.000 | 0.000 | -0.012 | 0.000 |
| IF | 858.000 | 4.500 | 0.000 | 8.318 | 0.000 | 0.000 | 0.000 | 0.000 | 0.009 | 0.000 |
| IF | 880.000 | 5.200 | 0.000 | 8.290 | 0.000 | 0.000 | 0.000 | 0.000 | 0.031 | 0.000 |
| IF | 894.000 | 5.600 | 0.000 | 8.273 | 0.000 | 0.000 | 0.000 | 0.000 | 0.010 | 0.000 |
| IF | 919.000 | 5.600 | 0.000 | 8.241 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| IF | 947.000 | 5.600 | 0.000 | 8.206 | 0.000 | 0.000 | 0.000 | 0.000 | -0.003 | 0.000 |
| IF | 958.000 | 5.500 | 0.000 | 8.192 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| IF | 977.000 | 5.600 | 0.000 | 8.168 | 0.000 | 0.000 | 0.000 | 0.000 | -0.016 | 0.000 |
| IF | 990.000 | 5.000 | 0.000 | 8.152 | 0.000 | 0.000 | 0.000 | 0.000 | -0.048 | 0.000 |
| IF | 1004.000 | 4.300 | 0.000 | 8.134 | 0.000 | 0.000 | 0.000 | 0.000 | -0.057 | 0.000 |
| IF | 1011.000 | 3.800 | 0.000 | 8.125 | 0.000 | 0.000 | 0.000 | 0.000 | -0.004 | 0.000 |
| IF | 1031.000 | 4.200 | 0.000 | 8.100 | 0.000 | 0.000 | 0.000 | 0.000 | 0.020 | 0.000 |
| ET | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

1

| | END STATION | END ELEVATION | FETCH LENGTH | SURGE ELEV 10-YEAR | SURGE ELEV 100-YEAR | INITIAL WAVE HEIGHT | INITIAL W. PERIOD | | BOTTOM SLOPE | AVERAGE A-ZONES |
|----|-------------|---------------|--------------|--------------------|---------------------|---------------------|-------------------|-------|--------------|-----------------|
| IE | 0.000 | 0.000 | 24.000 | 3.220 | 9.620 | 37.300 | 14.100 | 0.000 | 0.062 | 0.000 |
| IF | 8.000 | 0.500 | 0.000 | 9.602 | 0.000 | 0.000 | 0.000 | 0.000 | 0.090 | 0.000 |
| IF | 21.000 | 1.900 | 0.000 | 9.573 | 0.000 | 0.000 | 0.000 | 0.000 | 0.130 | 0.000 |
| IF | 28.000 | 3.100 | 0.000 | 9.558 | 0.000 | 0.000 | 0.000 | 0.000 | 0.138 | 0.000 |
| IF | 37.000 | 4.100 | 0.000 | 9.538 | 0.000 | 0.000 | 0.000 | 0.000 | 0.142 | 0.000 |
| IF | 40.000 | 4.800 | 0.000 | 9.531 | 0.000 | 0.000 | 0.000 | 0.000 | 0.130 | 0.000 |

| | | | | | | | | | | |
|----|---------------------------|---------------------------|-------------------------------|--------------------------------|-------|-------|-------|-------|---------------------------|-----------------------------|
| IF | END STATION 47.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.516 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.029 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 64.000 | END ELEVATION 5.500 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.478 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.004 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 75.000 | END ELEVATION 5.300 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.454 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.015 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 84.000 | END ELEVATION 5.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.434 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.007 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 89.000 | END ELEVATION 5.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.423 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.000 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 96.000 | END ELEVATION 5.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.407 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.000 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 103.000 | END ELEVATION 5.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.392 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.010 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 116.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.363 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.028 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 135.000 | END ELEVATION 6.100 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.321 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.027 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 142.000 | END ELEVATION 6.100 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.305 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.017 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 176.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.230 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.021 | AVERAGE A-ZONES 0.000 |
| AS | END STATION 182.000 | END ELEVATION 9.300 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.230 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.021 | AVERAGE A-ZONES 0.000 |
| AS | END STATION 185.000 | END ELEVATION 9.300 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.230 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.016 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 230.000 | END ELEVATION 8.600 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.156 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.016 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 254.000 | END ELEVATION 8.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.116 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.016 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 261.000 | END ELEVATION 8.100 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.105 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.004 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 276.000 | END ELEVATION 8.100 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.090 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.019 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 282.000 | END ELEVATION 7.700 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.073 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.075 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 288.000 | END ELEVATION 7.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.065 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.073 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 297.000 | END ELEVATION 6.600 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.054 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.037 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 307.000 | END ELEVATION 6.500 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.042 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.060 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 312.000 | END ELEVATION 7.500 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 9.036 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.030 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 354.000 | END ELEVATION 7.900 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.984 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.010 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 361.000 | END ELEVATION 7.000 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.976 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.070 | AVERAGE A-ZONES 0.000 |

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|----|---------------------------|---------------------------|-------------------------------|--------------------------------|-------|-------|-------|-------|---------------------------|-----------------------------|
| IF | END STATION 364.000 | END ELEVATION 7.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.972 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.070 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 371.000 | END ELEVATION 7.700 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.964 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.058 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 376.000 | END ELEVATION 7.900 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.958 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.018 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 382.000 | END ELEVATION 7.900 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.950 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.092 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 389.000 | END ELEVATION 6.700 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.942 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.211 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 391.000 | END ELEVATION 6.000 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.939 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.054 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 411.000 | END ELEVATION 5.500 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.915 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.016 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 428.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.894 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.004 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 458.000 | END ELEVATION 5.300 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.857 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.000 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 472.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.840 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.019 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 484.000 | END ELEVATION 4.800 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.823 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.038 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 493.000 | END ELEVATION 4.600 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.811 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.002 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 531.000 | END ELEVATION 4.900 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.759 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.007 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 583.000 | END ELEVATION 5.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.687 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.008 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 596.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.669 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.009 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 605.000 | END ELEVATION 5.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.657 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.021 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 615.000 | END ELEVATION 5.800 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.643 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.043 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 626.000 | END ELEVATION 6.300 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.628 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE 0.032 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 634.000 | END ELEVATION 6.400 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.617 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.007 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 640.000 | END ELEVATION 6.200 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.609 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.027 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 645.000 | END ELEVATION 6.100 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.602 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.030 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 650.000 | END ELEVATION 5.900 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.595 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.029 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 662.000 | END ELEVATION 5.600 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.578 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.046 | AVERAGE A-ZONES 0.000 |
| IF | END STATION 685.000 | END ELEVATION 4.300 | NEW SURGE 10-YEAR 0.000 | NEW SURGE 100-YEAR 8.547 | 0.000 | 0.000 | 0.000 | 0.000 | BOTTOM SLOPE -0.023 | AVERAGE A-ZONES 0.000 |

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|----|---------|------|------|------|
| IF | 696.00 | 0.93 | 1.15 | 9.19 |
| IF | 705.00 | 0.90 | 1.16 | 9.15 |
| IF | 717.00 | 0.93 | 1.16 | 9.15 |
| IF | 728.00 | 0.97 | 1.17 | 9.17 |
| IF | 744.00 | 1.00 | 1.18 | 9.17 |
| IF | 756.00 | 1.00 | 1.19 | 9.15 |
| IF | 766.00 | 1.03 | 1.20 | 9.15 |
| IF | 777.00 | 1.03 | 1.21 | 9.14 |
| IF | 802.00 | 1.08 | 1.22 | 9.15 |
| IF | 858.00 | 1.14 | 1.26 | 9.12 |
| IF | 880.00 | 1.14 | 1.27 | 9.09 |
| IF | 894.00 | 1.11 | 1.28 | 9.05 |
| IF | 919.00 | 1.13 | 1.30 | 9.03 |
| IF | 947.00 | 1.14 | 1.31 | 9.01 |
| IF | 958.00 | 1.16 | 1.32 | 9.00 |
| IF | 977.00 | 1.16 | 1.33 | 8.98 |
| IF | 990.00 | 1.23 | 1.33 | 9.01 |
| IF | 1004.00 | 1.27 | 1.34 | 9.02 |
| IF | 1011.00 | 1.29 | 1.35 | 9.03 |
| IF | 1031.00 | 1.30 | 1.36 | 9.01 |

TRANSMITTED WAVE HEIGHT AT LAST FETCH OR OBSTRUCTION = 1.30 WHICH EXCEEDS 0.5.

PART3 LOCATION OF AREAS ABOVE 100-YEAR SURGE

BETWEEN 176.00 AND 182.00
 BETWEEN 182.00 AND 185.00

PART4 LOCATION OF SURGE CHANGES

| STATION | 10-YEAR SURGE | 100-YEAR SURGE |
|---------|---------------|----------------|
| 0.00 | 3.22 | 9.60 |
| 21.00 | 3.22 | 9.57 |
| 28.00 | 3.22 | 9.56 |
| 37.00 | 3.22 | 9.54 |
| 40.00 | 3.22 | 9.53 |
| 47.00 | 3.22 | 9.52 |
| 64.00 | 3.22 | 9.48 |
| 75.00 | 3.22 | 9.45 |
| 84.00 | 3.22 | 9.43 |
| 89.00 | 3.22 | 9.42 |
| 96.00 | 3.22 | 9.41 |
| 103.00 | 3.22 | 9.39 |
| 116.00 | 3.22 | 9.36 |
| 135.00 | 3.22 | 9.32 |
| 142.00 | 3.22 | 9.31 |
| 176.00 | 3.22 | 9.23 |
| 230.00 | 3.22 | 9.16 |
| 254.00 | 3.22 | 9.12 |
| 261.00 | 3.22 | 9.10 |
| 276.00 | 3.22 | 9.08 |
| 282.00 | 3.22 | 9.07 |
| 288.00 | 3.22 | 9.06 |
| 297.00 | 3.22 | 9.05 |
| 307.00 | 3.22 | 9.04 |
| 312.00 | 3.22 | 9.04 |
| 354.00 | 3.22 | 8.98 |
| 361.00 | 3.22 | 8.98 |
| 364.00 | 3.22 | 8.97 |
| 371.00 | 3.22 | 8.96 |
| 376.00 | 3.22 | 8.96 |
| 382.00 | 3.22 | 8.95 |
| 389.00 | 3.22 | 8.94 |
| 391.00 | 3.22 | 8.94 |

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|---------|------|------|
| 411.00 | 3.22 | 8.91 |
| 428.00 | 3.22 | 8.89 |
| 458.00 | 3.22 | 8.86 |
| 472.00 | 3.22 | 8.84 |
| 484.00 | 3.22 | 8.82 |
| 493.00 | 3.22 | 8.81 |
| 531.00 | 3.22 | 8.76 |
| 583.00 | 3.22 | 8.69 |
| 596.00 | 3.22 | 8.67 |
| 605.00 | 3.22 | 8.66 |
| 615.00 | 3.22 | 8.64 |
| 626.00 | 3.22 | 8.63 |
| 634.00 | 3.22 | 8.62 |
| 640.00 | 3.22 | 8.61 |
| 645.00 | 3.22 | 8.60 |
| 650.00 | 3.22 | 8.60 |
| 662.00 | 3.22 | 8.58 |
| 685.00 | 3.22 | 8.55 |
| 688.00 | 3.22 | 8.54 |
| 691.00 | 3.22 | 8.54 |
| 696.00 | 3.22 | 8.53 |
| 705.00 | 3.22 | 8.52 |
| 717.00 | 3.22 | 8.50 |
| 728.00 | 3.22 | 8.49 |
| 744.00 | 3.22 | 8.47 |
| 756.00 | 3.22 | 8.45 |
| 766.00 | 3.22 | 8.44 |
| 777.00 | 3.22 | 8.42 |
| 802.00 | 3.22 | 8.39 |
| 858.00 | 3.22 | 8.32 |
| 880.00 | 3.22 | 8.29 |
| 894.00 | 3.22 | 8.27 |
| 919.00 | 3.22 | 8.24 |
| 947.00 | 3.22 | 8.21 |
| 958.00 | 3.22 | 8.19 |
| 977.00 | 3.22 | 8.17 |
| 990.00 | 3.22 | 8.15 |
| 1004.00 | 3.22 | 8.13 |
| 1011.00 | 3.22 | 8.12 |
| 1031.00 | 3.22 | 8.10 |

PART5 LOCATION OF V ZONES

| STATION OF GUTTER | LOCATION OF ZONE |
|-------------------|------------------|
| 118.40 | WINDWARD |

PART6 NUMBERED A ZONES AND V ZONES

| STATION OF GUTTER | ELEVATION | ZONE DESIGNATION | FHF |
|-------------------|-----------|------------------|-----|
| 0.00 | 14.80 | | |
| | | V20 EL=15 | 100 |
| 8.00 | 14.50 | | |
| | | V20 EL=15 | 100 |
| 8.04 | 14.50 | | |
| | | V20 EL=14 | 100 |
| 21.00 | 13.71 | | |
| | | V20 EL=14 | 100 |
| 23.25 | 13.50 | | |
| | | V20 EL=13 | 100 |
| 28.00 | 13.05 | | |
| | | V20 EL=13 | 100 |

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| | END STATION | END ELEVATION | NEW SURGE 10-YEAR | NEW SURGE 100-YEAR | | | | | | BOTTOM SLOPE | AVERAGE A-ZONES |
|----|----------------|------------------|----------------------|-----------------------|-------|-------|-------|-------|--|-----------------|--------------------|
| IF | 688.000 | 5.000 | 0.000 | 8.543 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.233 | 0.000 |
| IF | 691.000 | 5.700 | 0.000 | 8.538 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.112 | 0.000 |
| IF | 696.000 | 5.900 | 0.000 | 8.532 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.050 | 0.000 |
| IF | 705.000 | 6.400 | 0.000 | 8.519 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.014 | 0.000 |
| IF | 717.000 | 6.200 | 0.000 | 8.503 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.035 | 0.000 |
| IF | 728.000 | 5.600 | 0.000 | 8.487 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.033 | 0.000 |
| IF | 744.000 | 5.300 | 0.000 | 8.465 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.004 | 0.000 |
| IF | 756.000 | 5.700 | 0.000 | 8.449 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 |
| IF | 766.000 | 5.300 | 0.000 | 8.435 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.009 | 0.000 |
| IF | 777.000 | 5.500 | 0.000 | 8.420 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.022 | 0.000 |
| IF | 802.000 | 4.500 | 0.000 | 8.389 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.012 | 0.000 |
| IF | 858.000 | 4.500 | 0.000 | 8.318 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.009 | 0.000 |
| IF | 880.000 | 5.200 | 0.000 | 8.290 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.031 | 0.000 |
| IF | 894.000 | 5.600 | 0.000 | 8.273 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.010 | 0.000 |
| IF | 919.000 | 5.600 | 0.000 | 8.241 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 |
| IF | 947.000 | 5.600 | 0.000 | 8.206 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.003 | 0.000 |
| IF | 958.000 | 5.500 | 0.000 | 8.192 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 |
| IF | 977.000 | 5.600 | 0.000 | 8.168 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.016 | 0.000 |
| IF | 990.000 | 5.000 | 0.000 | 8.152 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.048 | 0.000 |
| IF | 1004.000 | 4.300 | 0.000 | 8.134 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.057 | 0.000 |
| IF | 1011.000 | 3.800 | 0.000 | 8.125 | 0.000 | 0.000 | 0.000 | 0.000 | | -0.004 | 0.000 |
| IF | 1031.000 | 4.200 | 0.000 | 8.100 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.020 | 0.000 |

-----END OF TRANSECT-----

NOTE:

SURGE ELEVATION INCLUDES CONTRIBUTIONS FROM ASTRONOMICAL AND STORM TIDES.

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PART2: CONTROLLING WAVE HEIGHTS, SPECTRAL
PEAK WAVE PERIOD, AND WAVE CREST ELEVATIONS

| LOCATION | CONTROLLING WAVE HEIGHT | SPECTRAL PEAK WAVE PERIOD | WAVE CREST ELEVATION |
|----------|----------------------------|------------------------------|-------------------------|
| IE | 0.00 | 7.39 | 14.10 |
| IF | 8.00 | 7.00 | 14.10 |
| IF | 21.00 | 5.91 | 14.10 |
| IF | 28.00 | 4.99 | 14.10 |
| IF | 37.00 | 4.21 | 14.10 |
| IF | 40.00 | 3.66 | 14.10 |
| IF | 47.00 | 3.19 | 14.10 |
| IF | 64.00 | 3.08 | 14.10 |
| IF | 75.00 | 3.12 | 14.10 |
| IF | 84.00 | 3.14 | 14.10 |
| IF | 89.00 | 3.14 | 14.10 |
| IF | 96.00 | 3.14 | 14.10 |
| IF | 103.00 | 3.14 | 14.10 |
| IF | 116.00 | 3.07 | 14.10 |
| IF | 135.00 | 2.50 | 14.10 |
| IF | 142.00 | 2.49 | 14.10 |
| IF | 176.00 | 2.61 | 14.10 |
| AS | 182.00 | 0.00 | 0.00 |
| AS | 185.00 | 0.00 | 0.00 |
| IF | 230.00 | 0.19 | 0.51 |
| IF | 254.00 | 0.25 | 0.59 |
| IF | 261.00 | 0.27 | 0.61 |
| IF | 276.00 | 0.30 | 0.65 |
| IF | 282.00 | 0.32 | 0.66 |
| IF | 288.00 | 0.33 | 0.68 |
| IF | 297.00 | 0.35 | 0.69 |
| IF | 307.00 | 0.37 | 0.71 |
| IF | 312.00 | 0.38 | 0.72 |
| IF | 354.00 | 0.43 | 0.80 |
| IF | 361.00 | 0.47 | 0.81 |
| IF | 364.00 | 0.48 | 0.81 |
| IF | 371.00 | 0.47 | 0.82 |
| IF | 376.00 | 0.46 | 0.83 |
| IF | 382.00 | 0.46 | 0.84 |
| IF | 389.00 | 0.52 | 0.85 |
| IF | 391.00 | 0.53 | 0.85 |
| IF | 411.00 | 0.56 | 0.88 |
| IF | 428.00 | 0.59 | 0.90 |
| IF | 458.00 | 0.64 | 0.93 |
| IF | 472.00 | 0.66 | 0.95 |
| IF | 484.00 | 0.68 | 0.96 |
| IF | 493.00 | 0.69 | 0.97 |
| IF | 531.00 | 0.75 | 1.01 |
| IF | 583.00 | 0.82 | 1.06 |
| IF | 596.00 | 0.83 | 1.07 |
| IF | 605.00 | 0.84 | 1.08 |
| IF | 615.00 | 0.85 | 1.09 |
| IF | 626.00 | 0.84 | 1.09 |
| IF | 634.00 | 0.84 | 1.10 |
| IF | 640.00 | 0.86 | 1.11 |
| IF | 645.00 | 0.87 | 1.11 |
| IF | 650.00 | 0.88 | 1.11 |
| IF | 662.00 | 0.91 | 1.12 |
| IF | 685.00 | 0.95 | 1.14 |
| IF | 688.00 | 0.95 | 1.14 |
| IF | 691.00 | 0.94 | 1.15 |

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| | | | | |
|--------|-------|-----|-------|-----|
| 36.72 | 12.50 | V20 | EL=12 | 100 |
| 37.00 | 12.48 | V20 | EL=12 | 100 |
| 40.00 | 12.10 | V19 | EL=12 | 95 |
| 47.00 | 11.75 | V19 | EL=12 | 95 |
| 64.00 | 11.64 | V19 | EL=12 | 95 |
| 75.00 | 11.64 | V19 | EL=12 | 95 |
| 84.00 | 11.63 | V19 | EL=12 | 95 |
| 89.00 | 11.62 | V19 | EL=12 | 95 |
| 96.00 | 11.61 | V19 | EL=12 | 95 |
| 103.00 | 11.59 | V19 | EL=12 | 95 |
| 116.00 | 11.51 | V19 | EL=12 | 95 |
| 116.58 | 11.50 | V19 | EL=11 | 95 |
| 118.40 | 11.44 | A12 | EL=11 | 60 |
| 135.00 | 11.07 | A12 | EL=11 | 60 |
| 142.00 | 11.05 | A12 | EL=11 | 60 |
| 176.00 | 11.06 | | | |
| 182.00 | 9.30 | | | |
| 185.00 | 9.30 | A12 | EL= 9 | 60 |
| 230.00 | 9.29 | A12 | EL= 9 | 60 |
| 254.00 | 9.29 | A12 | EL= 9 | 60 |
| 261.00 | 9.29 | A12 | EL= 9 | 60 |
| 276.00 | 9.29 | A12 | EL= 9 | 60 |
| 282.00 | 9.30 | A12 | EL= 9 | 60 |
| 288.00 | 9.30 | A12 | EL= 9 | 60 |
| 297.00 | 9.30 | A12 | EL= 9 | 60 |
| 307.00 | 9.30 | A12 | EL= 9 | 60 |
| 312.00 | 9.30 | A12 | EL= 9 | 60 |
| 354.00 | 9.29 | A12 | EL= 9 | 60 |
| 361.00 | 9.31 | A12 | EL= 9 | 60 |
| 364.00 | 9.31 | A12 | EL= 9 | 60 |
| 371.00 | 9.29 | | | |

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| | | | | |
|--------|------|-----|-------|----|
| | | A12 | EL= 9 | 60 |
| 376.00 | 9.28 | | | |
| | | A12 | EL= 9 | 60 |
| 382.00 | 9.27 | | | |
| | | A12 | EL= 9 | 60 |
| 389.00 | 9.31 | | | |
| | | A12 | EL= 9 | 60 |
| 391.00 | 9.31 | | | |
| | | A12 | EL= 9 | 60 |
| 411.00 | 9.31 | | | |
| | | A12 | EL= 9 | 60 |
| 428.00 | 9.31 | | | |
| | | A12 | EL= 9 | 60 |
| 458.00 | 9.30 | | | |
| | | A12 | EL= 9 | 60 |
| 472.00 | 9.30 | | | |
| | | A12 | EL= 9 | 60 |
| 484.00 | 9.30 | | | |
| | | A12 | EL= 9 | 60 |
| 493.00 | 9.29 | | | |
| | | A12 | EL= 9 | 60 |
| 531.00 | 9.28 | | | |
| | | A12 | EL= 9 | 60 |
| 583.00 | 9.26 | | | |
| | | A12 | EL= 9 | 60 |
| 596.00 | 9.25 | | | |
| | | A12 | EL= 9 | 60 |
| 605.00 | 9.25 | | | |
| | | A12 | EL= 9 | 60 |
| 615.00 | 9.24 | | | |
| | | A12 | EL= 9 | 60 |
| 626.00 | 9.22 | | | |
| | | A12 | EL= 9 | 60 |
| 634.00 | 9.21 | | | |
| | | A12 | EL= 9 | 60 |
| 640.00 | 9.21 | | | |
| | | A12 | EL= 9 | 60 |
| 645.00 | 9.21 | | | |
| | | A12 | EL= 9 | 60 |
| 650.00 | 9.22 | | | |
| | | A12 | EL= 9 | 60 |
| 662.00 | 9.21 | | | |
| | | A12 | EL= 9 | 60 |
| 685.00 | 9.21 | | | |
| | | A12 | EL= 9 | 60 |
| 688.00 | 9.21 | | | |
| | | A12 | EL= 9 | 60 |
| 691.00 | 9.19 | | | |
| | | A12 | EL= 9 | 60 |
| 696.00 | 9.19 | | | |
| | | A12 | EL= 9 | 60 |
| 705.00 | 9.15 | | | |
| | | A12 | EL= 9 | 60 |
| 717.00 | 9.15 | | | |
| | | A12 | EL= 9 | 60 |
| 728.00 | 9.17 | | | |
| | | A12 | EL= 9 | 60 |
| 744.00 | 9.17 | | | |
| | | A12 | EL= 9 | 60 |
| 756.00 | 9.15 | | | |

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| | | | |
|---------|------|-----------|----|
| | | A12 EL= 9 | 60 |
| 766.00 | 9.15 | | |
| | | A12 EL= 9 | 60 |
| 777.00 | 9.14 | | |
| | | A12 EL= 9 | 60 |
| 802.00 | 9.15 | | |
| | | A12 EL= 9 | 60 |
| 858.00 | 9.12 | | |
| | | A12 EL= 9 | 60 |
| 880.00 | 9.09 | | |
| | | A12 EL= 9 | 60 |
| 894.00 | 9.05 | | |
| | | A12 EL= 9 | 60 |
| 919.00 | 9.03 | | |
| | | A12 EL= 9 | 60 |
| 947.00 | 9.01 | | |
| | | A12 EL= 9 | 60 |
| 958.00 | 9.00 | | |
| | | A12 EL= 9 | 60 |
| 977.00 | 8.98 | | |
| | | A12 EL= 9 | 60 |
| 990.00 | 9.01 | | |
| | | A12 EL= 9 | 60 |
| 1004.00 | 9.02 | | |
| | | A12 EL= 9 | 60 |
| 1011.00 | 9.03 | | |
| | | A12 EL= 9 | 60 |
| 1031.00 | 9.01 | | |

ZONE TERMINATED AT END OF TRANSECT

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